

# Darmstadt Lecture 3 – Nuclear Structure

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# Nuclear Symmetry Energy

Defined as the difference between energies of pure neutron matter ( $x = 0$ ) and symmetric ( $x = 1/2$ ) nuclear matter.

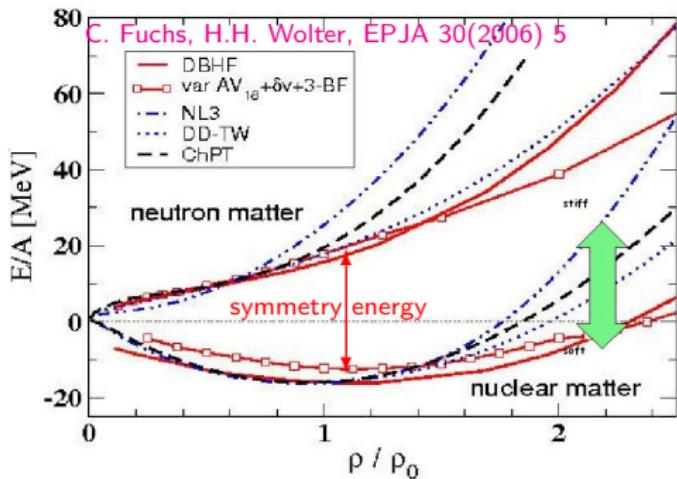
$$S(\rho) = E(\rho, x = 0) - E(\rho, x = 1/2)$$

Expanding around saturation density ( $\rho_s$ ) and symmetric matter ( $x = 1/2$ )

$$E(\rho, x) = E(\rho, 1/2) + (1-2x)^2 S_2(\rho) + \dots$$

$$S_2(\rho) = \mathbf{S}_v + \frac{\mathbf{L}}{3} \frac{\rho - \rho_s}{\rho_s} + \dots$$

$$\mathbf{S}_v \simeq 31 \text{ MeV}, \mathbf{L} \simeq 50 \text{ MeV}$$



Connections to neutron matter:

$$E(\rho_s, 0) \approx S_v + E(\rho_s, 1/2) = S_v - B, \quad p(\rho_s, 0) = L\rho_s/3$$

Neutron star matter (in beta equilibrium):

$$\frac{\partial(E + E_e)}{\partial x} = 0, \quad p(\rho_s, x_\beta) \simeq \frac{L\rho_s}{3} \left[ 1 - \left( \frac{4S_v}{\hbar c} \right)^3 \frac{4 - 3S_v/L}{3\pi^2\rho_s} \right]$$

# Nuclear Mass Formula

Bethe-Weizsäcker (neglecting pairing and shell effects)

$$E(A, Z) = -a_v A + a_s A^{2/3} + a_c Z^2 / A^{1/3} + S_v A I^2.$$

Myers & Swiatecki introduced the surface asymmetry term:

$$E(A, Z) = -a_v A + a_s A^{2/3} + a_c Z^2 / A^{1/3} + S_v A I^2 - S_s (N - Z)^2 / A^{4/3}.$$

$a_v = B$ ,  $a_s \simeq 18$  MeV,  $a_c \simeq 0.75$  MeV,  $S_s \simeq 45$  MeV,  $I = (N - Z)/A$

Optimum Nucleus

$$\begin{aligned}\frac{\partial E/A}{\partial A} &= -\frac{a_s}{3} A^{-4/3} + \frac{a_c}{6} A^{-1/3} (1 - I)^2 - \frac{S_s}{3} I^2 A^{-4/3} = 0 \\ \frac{\partial E/A}{\partial I} &= \frac{-a_c}{2} A^{2/3} (1 - I) + 2S_v I - 2S_s A^{-1/3} I\end{aligned}$$

$$A = \frac{2(a_s + S_s I^2)}{a_c (1 - I)^2} \sim 48(1 - I)^{-2} \sim 57$$

$$I = \frac{a_c}{4S_v A^{-2/3} - 2S_s/A + a_c} \sim \frac{1}{12}$$

# Nuclei at High Densities From Liquid Drop

$$E(Z, N) \simeq -BA + S_v Al^2 + (E_s - S_s l^2) A^{2/3} + E_C \frac{Z^2}{A^{1/3}}$$

$B \simeq 16$  MeV,  $S_v \simeq 30$  MeV,  $E_s \simeq 18$  MeV,  $S_s \simeq 45$  MeV,  $E_C \simeq 0.75$  MeV.

At each density, the preferred nucleus has a mass determined by

$$\left( \frac{\partial(E/A)}{\partial A} \right)_x = -\frac{E_s - S_s l^2}{3A^{4/3}} + \frac{2E_C x^2}{3A^{1/3}} = 0$$

. The Nuclear Virial Theorem is

$$E_s - S_s l^2 = 2E_C x^2 A, \quad A_{opt} = 2 \frac{E_s - S_s l^2}{E_C (1 - l)^2} \simeq 48(1 + 2l) \simeq 61.$$

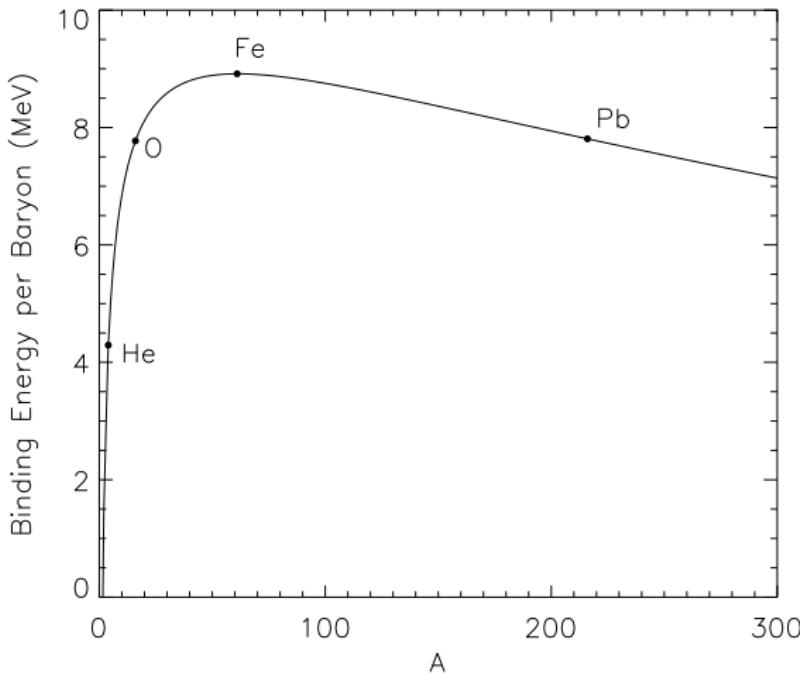
At low densities, the optimum nucleus has a charge determined by

$$\left( \frac{\partial(E/A)}{\partial x} \right)_A = -4l \left( S_v - \frac{S_s}{A^{1/3}} \right) + (1 - l) E_C A^{2/3} = 0,$$
$$l = \frac{E_C A}{4(S_v A^{1/3} - S_s) + E_C A} \simeq 0.125; \quad Z \simeq 27$$

# Isolated Nuclei

The binding energy curve is heavily skewed. Certain closed-shell nuclei (He, C, O, Pb) have much larger binding than the average.

The optimum value of  $I$  increases with mass number  $A$ . This trend represents the *Valley of Beta Stability*.



# Nuclei at Higher Densities

At the end of stellar evolution, when an iron core forms, the central stellar density is about  $\rho \simeq 10^7 \text{ g cm}^{-3}$ , implying a filling factor  $u = \rho/\rho_s \simeq 3.7 \cdot 10^{-8}$ . The intranuclear spacing is about  $2u^{-1/3} \simeq 600$  nuclear radii.

Electron screening reduces the nuclear Coulomb energy.

Approximating electrons as uniformly distributed, even within nuclei, the nuclear Coulomb energy is:

$$E_{Coul} = \frac{3}{5} \frac{Z^2 e^2}{R} \left( 1 - \frac{3}{2} u^{1/3} + \frac{u}{2} \right)$$

The reduction factor is about 0.5% for  $\rho \simeq 10^7 \text{ g cm}^{-3}$ .

This effect increases the nuclear mass, which is proportional to  $E_{Coul}^{-1}$ , as the average density increases.

The optimum  $I$  also increases with density due to *beta equilibrium*:

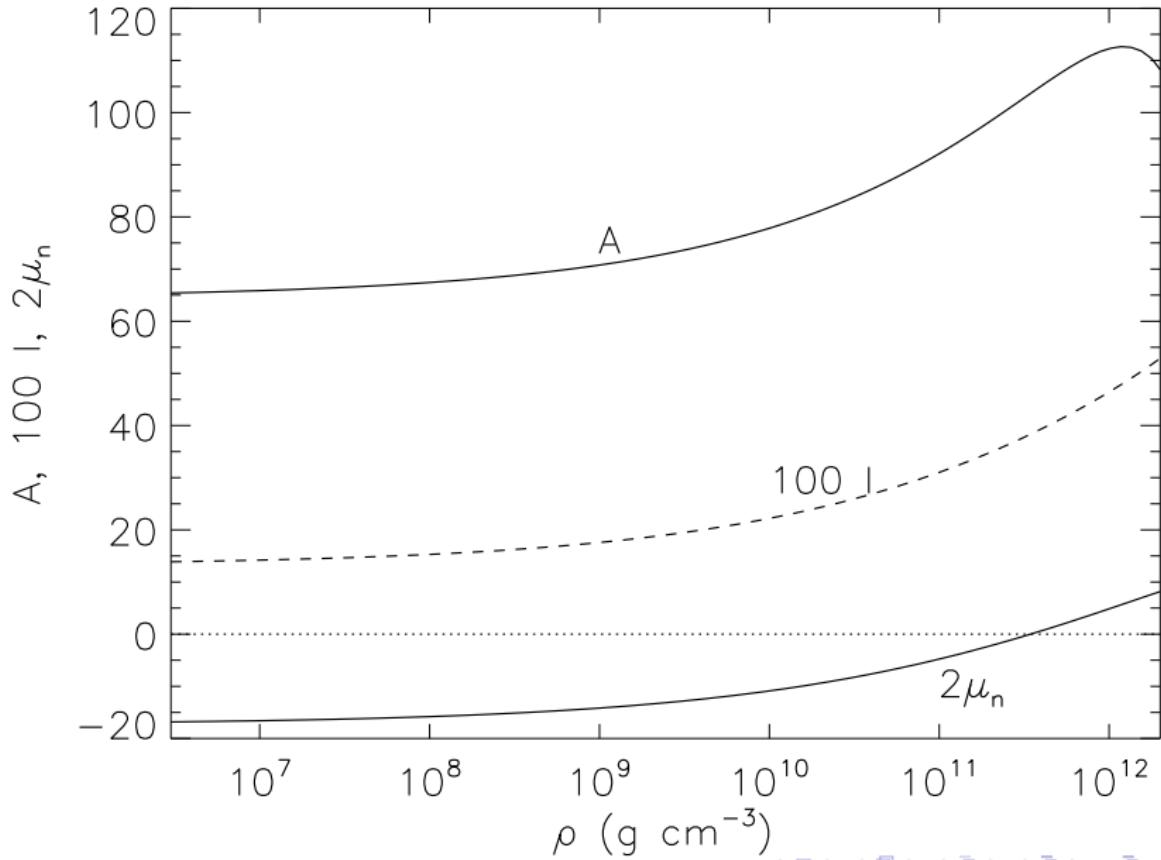
$$\frac{\partial(E/A + E_e)}{\partial x} = -\mu_n + \mu_p + \mu_e = 0.$$

# Chemical Potentials and Neutron Drip

Chemical potentials are equivalent to the separation energies:

$$\begin{aligned}\mu_n &= \left( \frac{\partial(E/A)}{\partial N} \right)_Z, & \mu_p &= \left( \frac{\partial(E/A)}{\partial Z} \right)_N, \\ \mu_e &= \frac{\partial(E_e n Y_e)}{\partial(n Y_e)} = \hbar c (3\pi^2 n_s u x)^{1/3}, & Y_e &= x, \\ \mu_n - \mu_p &= - \left( \frac{\partial(E/A)}{\partial x} \right)_A,\end{aligned}$$

At sufficiently high density, about  $\rho = (3.5 - 4) \cdot 10^{11} \text{ g cm}^{-3}$ , as  $x$  becomes smaller and  $A$  becomes larger,  $\mu_n$  becomes positive. Neutrons thus 'drip' out of nuclei.



# Nuclear Droplet Model

Myers & Swiatecki droplet extension: consider the variation of the neutron/proton asymmetry within the nuclear surface.

$$E(A, Z) = (-B + S_v \delta^2)(A - N_s) + (E_s - S_s \delta^2)A^{2/3} + E_c Z^2 A^{-1/3} + \mu_n N_s.$$

$N_s$  is the number of excess neutrons associated with the surface,

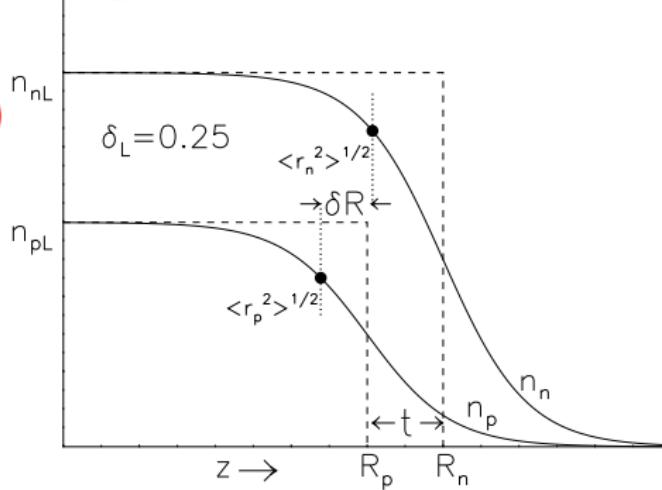
$$\delta = 1 - 2x = (A - N_s - 2Z)/(A - N_s)$$

is the asymmetry of the nuclear bulk fluid, and  $\mu_n = -a_v + S_v \delta(2 - \delta)$  is the neutron chemical potential.

Surface tension is the surface thermodynamic potential; adding  $\mu_n N_s$  gives the total surface energy. Optimizing  $E(A, Z)$  with respect to  $N_s$  yields

$$N_s = \frac{S_s}{S_v} \frac{\delta}{1 - \delta} = A \frac{I - \delta}{1 - \delta}, \quad \delta = I \left( 1 + \frac{S_s}{S_v A^{1/3}} \right)^{-1},$$

$$E(A, Z) = -BA + E_s A^{2/3} + E_c Z^2 / A^{1/3} + S_v A I^2 \left( 1 + \frac{S_s}{S_v A^{1/3}} \right)^{-1}.$$



# Macroscopic Hydrodynamic Nuclear Model

$$\mathcal{H} = \mathcal{H}_B(n, \alpha) + \mathcal{H}_C(n, \alpha) + \mathcal{Q}(n)(n')^2, \quad \mathcal{H}_B(n, \alpha) = \mathcal{H}_B(n, 0) + v_{sym}(n)\alpha^2$$

$$\alpha = n_n - n_p, \quad n' = dn/dr, \quad v_{sym} = S_2(n)/n, \quad \mathcal{H}_C = n_p V_C/2$$

$$V_C(r) = \frac{e^2}{r} \int_0^r n_p(r') d^3 r' + \int_r^\infty \frac{e^2}{r'} n_p(r') d^3 r' \simeq \frac{Ze^2}{R} \left( \frac{3}{2} - \frac{r^2}{2R^2} \right)$$

Optimize total energy with respect to  $n$  and  $\alpha$  subject to fixed

$A = \int \rho d^3 r$  and  $N - Z = \int \alpha d^3 r$ :

$$\frac{\delta}{\delta n} [\mathcal{H} - \mu n] = 0, \quad \frac{\delta}{\delta \alpha} [\mathcal{H} - \bar{\mu} \alpha] = 0.$$

$$\mu = \frac{\partial [\mathcal{H}_B + \mathcal{H}_C]}{\partial n} = 2 \frac{d}{dr} [\mathcal{Q} n'] + \frac{\partial \mathcal{Q}}{\partial n} (n')^2, \quad \bar{\mu} = \frac{\partial [\mathcal{H}_B + \mathcal{H}_C]}{\partial \alpha}$$

Multiply first by  $n'$  and second by  $\alpha'$  and add, then integrate once:

$$\mathcal{Q}(n)(n')^2 = \mathcal{H}_B + \mathcal{H}_C - \mu n - \bar{\mu} \alpha$$

# Surface Energy

Consider a symmetric, chargeless nucleus. The total energy, the sum of volume and surface energies, is

$$\int \mathcal{H} d^3r = \mu A + \int [\mathcal{H} - \mu n] d^3r \simeq \mu A + 4\pi R^2 \int_{-\infty}^{\infty} [\mathcal{H} - \mu n] dx$$

We made a *leptodermous expansion* above to isolate the surface.

$$E_{vol,o} + E_{surf,o} = \mu A + 4\pi R^2 \int [\mathcal{H}_B(n, 0) - \mu n + \mathcal{Q}(n)(n')^2] dx$$

Assume  $\mathcal{H}_B(n, 0) = n\mu + (nK_s/18)(1-u)^2$ ,  $u = n/n_s$ ,  $\mathcal{Q}(n) = Q/n$ ,  $\mu = -B$ :

$$\frac{du}{dz} = -u(1-u), \quad z = \frac{x}{a}, \quad a = \sqrt{\frac{18Q}{K_s}}, \quad u = \frac{1}{1 + e^{z-y}}$$

$$A = 4\pi n_s a^3 F_2(y), \quad F_i(y) = \int_0^\infty \frac{z^i dz}{1 + e^{z-y}} \simeq \frac{y^{i+1}}{i+1} \left[ 1 + \frac{i(i+1)}{6} \left( \frac{\pi}{y} \right)^2 + \dots \right]$$

This determines the parameter  $y \approx R/a$ , which is related to the radius.

The surface tension for symmetric matter is

$$\sigma_o = \frac{E_{surf,o}}{4\pi R^2} = 2Q \int_0^\infty \left( \frac{dn}{dz} \right)^2 \frac{dz}{n} = 2Q \int_{n_s}^0 \frac{dn}{dz} \frac{dn}{n} = \frac{Q n_s}{a}$$

Parameter determination:

$$t_{90-10} = a \int_{0.1}^{0.9} \frac{dz}{du} du = 4a \ln 3 = 2.3 \text{ fm}, \quad a \simeq 0.523 \text{ fm}$$

$$Q = \frac{K_s}{18} \left( \frac{t_{90-10}}{4 \ln 3} \right)^2 \simeq 3.65 \text{ MeV fm}^2, \quad K_s = 240 \text{ MeV}$$

$$\begin{aligned} \sigma_o &= \int [\mathcal{H} - \mu n] dx = 2Q \int_0^\infty \frac{(n')^2}{n} dx = 2Q \int_{n_s}^0 \frac{n'}{n} dn \\ &= \frac{Q n_s}{a} \simeq 1.17 \text{ MeV fm}^{-2} \end{aligned}$$

$$E_s = 4\pi r_o^2 \sigma_o \simeq 19.2 \text{ MeV}, \quad r_o = \left( \frac{3}{4\pi n_s} \right)^{1/3} \simeq 1.143 \text{ fm}$$

# Determination of Isovector Density $\alpha$

$$\alpha = \frac{\bar{\mu} + \partial \mathcal{H}_C / \partial \alpha}{2v_{sym}} = \frac{\bar{\mu} + V_C/2}{v_{sym}}$$

$$N - Z = IA = \int \frac{\bar{\mu} + V_C/2}{2v_{sym}} d^3r \equiv \frac{\bar{\mu}}{2} H_0 + \frac{G}{4}$$

$$H_i = \int \left( \frac{r}{R} \right)^i \frac{d^3r}{v_{sym}}, \quad G = \frac{V_C}{v_{sym}} d^3r = \frac{Ze^2}{2R} (3H_0 - H_2)$$

$$\alpha = \frac{N - Z - (G - V_C H_0)/4}{v_{sym} H_0}$$

$$\alpha_o = \frac{n_s}{S_v H_0} \left( N - Z + \frac{Ze^2}{8R} H_2 \right), \quad v_{sym}(n_s) = \frac{S_v}{n_s}$$

Polarization results in an increase in asymmetry near the center.

# Nuclear Structure

Total symmetry and Coulomb energy:

$$\begin{aligned} E_{sym} + E_C &= \int v_{sym} \alpha^2 d^3 r + \frac{1}{4} \int (n - \alpha) V_C d^3 r \\ &= \frac{(N - Z)^2}{H_0} - \frac{(N - Z) G}{4 H_0} + \frac{1}{4} \int n V_C d^3 r \\ &= \frac{(N - Z)^2}{H_0} + \frac{3}{5} \frac{Z^2 e^2}{R} + \frac{Ze^2}{8R} (N - Z) \left( \frac{H_s}{H_0} - \frac{3}{5} \right) \end{aligned}$$

Dipole polarizability  $\alpha_D$ :

$$\frac{\delta}{\delta \alpha} \left( \int \mathcal{H} d^3 r - \epsilon \int z \alpha d^3 r \right) = 0$$

$\alpha_d$  is the function  $\alpha(r)$  which solves this.

$$\alpha_d = \frac{\epsilon z + V_C}{2v_{sym}}$$

$$\alpha_D = \frac{1}{2\epsilon} \int z \alpha_d d^3 r = \frac{1}{4\epsilon} \int z \frac{\epsilon z + V_C}{v_{sym}} d^3 r = \frac{R^2 H_2}{12}$$

# Neutron Skin Thickness

$$\begin{aligned}\frac{4\pi}{3} (R_n^3 - R_p^3) &= \int \left( \frac{n_n}{n_{no}} - \frac{n_p}{n_{po}} \right) d^3r = \frac{n_s}{2n_{no}n_{po}} \int \left( \alpha - n \frac{\alpha_o}{n_s} \right) d^3r \\ &= \frac{n_s A}{2n_{no}n_{po}} \left( I - \frac{\alpha_o}{n_s} \right) \\ \frac{R_n - R_p}{R} &\simeq \frac{2}{3} \frac{I - \alpha_o/n_s}{1 - \alpha_o^2/n_s^2} = \frac{2}{3} \left[ I \left( 1 - \frac{A}{S_v H_0} \right) - \frac{Ze^2}{8RS_v} \frac{H_2}{H_0} \right]\end{aligned}$$

Polarization decreases neutron skin thickness.

Symmetric nuclei have a proton skin.

$$\begin{aligned}r_{n,p}^2 &= \frac{1}{(N,Z)} \int n_{n,p} r^2 d^3r = \frac{1}{2(N,Z)} \int (n \pm \alpha) r^2 d^3r \\ &= \frac{R^2}{1 \pm I} \left[ \frac{3}{5} \pm \left( I \frac{H_2}{H_0} - \frac{Ze^2}{8RA} \left[ H_4 - \frac{H_2^2}{H_0} \right] \right) \right]\end{aligned}$$

$$\frac{r_{np}}{R} \equiv \frac{r_n - r_p}{R} = \sqrt{\frac{3}{5}} \left[ I \left( \frac{5H_2}{3H_0} - 1 \right) - \frac{5Ze^2}{24RA} \left( H_4 - \frac{H_2^2}{H_0} \right) \right] \frac{1}{\sqrt{1 - I^2}}$$

# Solutions for Arbitrary $v_{sym}$

Assume  $v_{sym}$  can be expanded as

$$\frac{S_v}{n_s v_{sym}(u)} = \sum_{j=1}^J b_j u^j, \quad 0 < u < 1$$

If the density has the Fermi shape, we find

$$H_i = \int \left(\frac{r}{R}\right)^i \frac{d^3 r}{v_{sym}} = \frac{4\pi n_s a^{3+i}}{S_v R^i} [F_{i+2}(y) - (2+i)\mathcal{T}F_{i+1}(y) + \dots]$$

$$\mathcal{T} = b_2 + \frac{3}{2}b_3 + \frac{11}{5}b_4 + \frac{25}{12}b_5 + \frac{137}{60}b_6 + \dots$$

$\sum_{j=1}^J b_j = 1$  ensures that  $v_{sym}(u=1) = S_v/n_s$ .

Noting that in the droplet model  $E_{sym} = S_v A l^2 (1 + S_s A^{-1/3}/S_v)^{-1}$  and in this model  $E_{sym} = A^2 l^2 / H_0$ , identify

$$H_0 = \frac{A}{S_v} \left(1 + \frac{S_s}{S_v A^{1/3}}\right) \simeq \frac{A}{S_v} \left(1 - \frac{3\mathcal{T}a}{r_o A^{1/3}}\right)$$

so that  $S_s \simeq -3\mathcal{T}S_v a/r_o$ .

It now follows that

$$H_i \simeq \frac{A}{S_v} \left( \frac{3}{3+i} + \frac{S_s}{S_v A^{1/3}} \right)$$

$$\alpha_D \simeq \frac{AR^2}{20S_v} \left( 1 + \frac{5}{3} \frac{S_s}{S_v A^{1/3}} \right)$$

$$r_{np} \simeq \sqrt{\frac{3}{5(1-I^2)}} \frac{2r_o}{3} \left( 1 + \frac{S_s}{S_v A^{1/3}} \right)^{-1} \left[ I \frac{S_s}{S_v} - \frac{3Ze^2}{140r_o S_v} \left( 1 + \frac{10}{3} \frac{S_s}{S_v A^{1/3}} \right) \right]$$

As an example, consider the expansion

$$S_2(u) \simeq S_v + \frac{L}{3}(u-1) + \frac{K_{sym}}{18}(u-1)^2 + \dots, \quad K_{sym} \simeq 18 \left( \frac{L}{3} - S_v \right)$$

To leading order, one finds  $S_s/S_v \simeq 1.35$

$$b_1 = 1 + \frac{L}{3S_v} + \left( \frac{L}{3S_v} \right)^2 - \frac{K_{sym}}{18S_v} \simeq 2.37$$

$$b_2 = \frac{K_{sym}}{9S_v} - \frac{L}{3S_v} - 2 \left( \frac{L}{3S_v} \right)^2 \simeq -2.14 \quad b_3 = \left( \frac{L}{3S_v} \right)^2 - \frac{K_{sym}}{18S_v} \simeq -0.76$$

$$\mathcal{T} = -\frac{L}{3S_v} - \frac{1}{2} \left( \frac{L}{3S_v} \right)^2 + \frac{K_{sym}}{36S_v} = -\frac{1}{2} \left[ 1 + \frac{L}{3S_v} + \left( \frac{L}{3S_v} \right)^2 \right] \simeq -0.992$$